



Determination of total organic carbon content using Passey's method in coals of the central Kalahari Karoo Basin, Botswana

Mamphedi Sylvia Mabitje, Mimonitu Opuwari*

Petroleum Geoscience Research Group, Department of Earth Sciences, University of the Western Cape, Cape Town, South Africa

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ABSTRACT

This paper focuses on determining total organic carbon (TOC) from boreholes in the Kalahari Basin, Botswana, using Passey's method. The Kalahari Karoo basin is one of several basins in southern Africa filled with Late Carboniferous to Jurassic sedimentary strata that host Permian age coal seams. Nine exploration boreholes (wells) drilled in the central Kalahari Karoo basin are used to determine the Total Organic Carbon potential. Vitrinite reflectance (R_o), proximate and ultimate analyses were conducted on cored coal intervals. Passey's ΔLogR method applied in this study employs resistivity and porosity logs to identify and quantify potential source rocks. Results of Passey's method compared with laboratory-measured carbon showed that Passey's method effectively identifies coal intervals. In terms of TOC calculations, the method works poorly in coal metamorphosed by dolerite intrusions. The heat affected coal samples had R_o from 0.77% to 5.53% and increased in maturity from primarily maceral controlled to high volatile bituminous and anthracite coal. Results from proximate analysis showed compositional changes in the coal were controlled by proximity to sill intrusion, with a decrease in Fixed Carbon and an increase in ash yield in the contact metamorphism zone (2–12 m from sill). For the unaltered coal that has undergone burial maturation displaying R_o of 0.44%–0.65%, the method works well. In unintruded boreholes, correlations between Carbon and calculated TOC indicate strong relationships. Passey's ΔLogR method proved to be a suitable method of estimating TOC on coal that has undergone burial maturation. This study has demonstrated that TOC calculated from the sonic log is more reliable in coal not affected by contact metamorphism than TOC calculated from the density log.

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1. Introduction

Total Organic Carbon (TOC) content estimation is an essential component in source rock evaluation (Fertl and Chilingar, 1988; Kamali and Mirshady, 2004; Amiri Bakhtiar et al., 2011; Jarvie, 2012; Wang et al., 2016; Nyakilla et al., 2022). One of the indirect methods for the determination of TOC from well logs is from Passey's 1990 approach. The TOC content can also be used to determine fluid saturation and porosity in the formation evaluation because of the effects of organic matter on reservoir properties (Passey et al., 1990; Sondergeld et al., 2010; Alfred and Vernik, 2012; Li et al., 2014; Zhao et al., 2017).

Coal type refers to coals depositional origin and the maceral–mineral admixture resulting from that origin. Coal types

typically fall into two categories: humic coals, developed from peat, and sapropelic coals, created from organic mud (O'Keefe et al., 2013). Shale in kerogen type is increasingly becoming an exploration target in many basins across the world as a potentially significant hydrocarbon generating source (Singh and Singh, 1994; Ogala, 2011; Singh, 2012; Zhang et al., 2018; Akanksha et al., 2020; Mohammed et al., 2019, 2020; Panwar et al., 2020). Kubu Energy acquired coal prospecting licences for three blocks (Fig. 1) within the Central Kalahari Karoo Basin, Botswana. Exploration in the basin revealed that methane concentrations in the coal seams of the Morupule and Serowe Formations' are under-saturated. Desorbed gas contents range between <1 and ≈ 2 m³/t, with a few higher readings associated with dolerite intrusions (Faiz et al., 2013).

Coal bed methane (CBM) is also known as coal seam gas (CSG), coal seam methane (CSM), and coal seam natural gas (CSNG). CBM forms as a thermogenically or biogenically derived gas (Moore, 2012). Methane occurs within the coal seam as adsorbed gas

* Corresponding author.

E-mail address: mopuwari@uwc.ac.za (M. Opuwari).

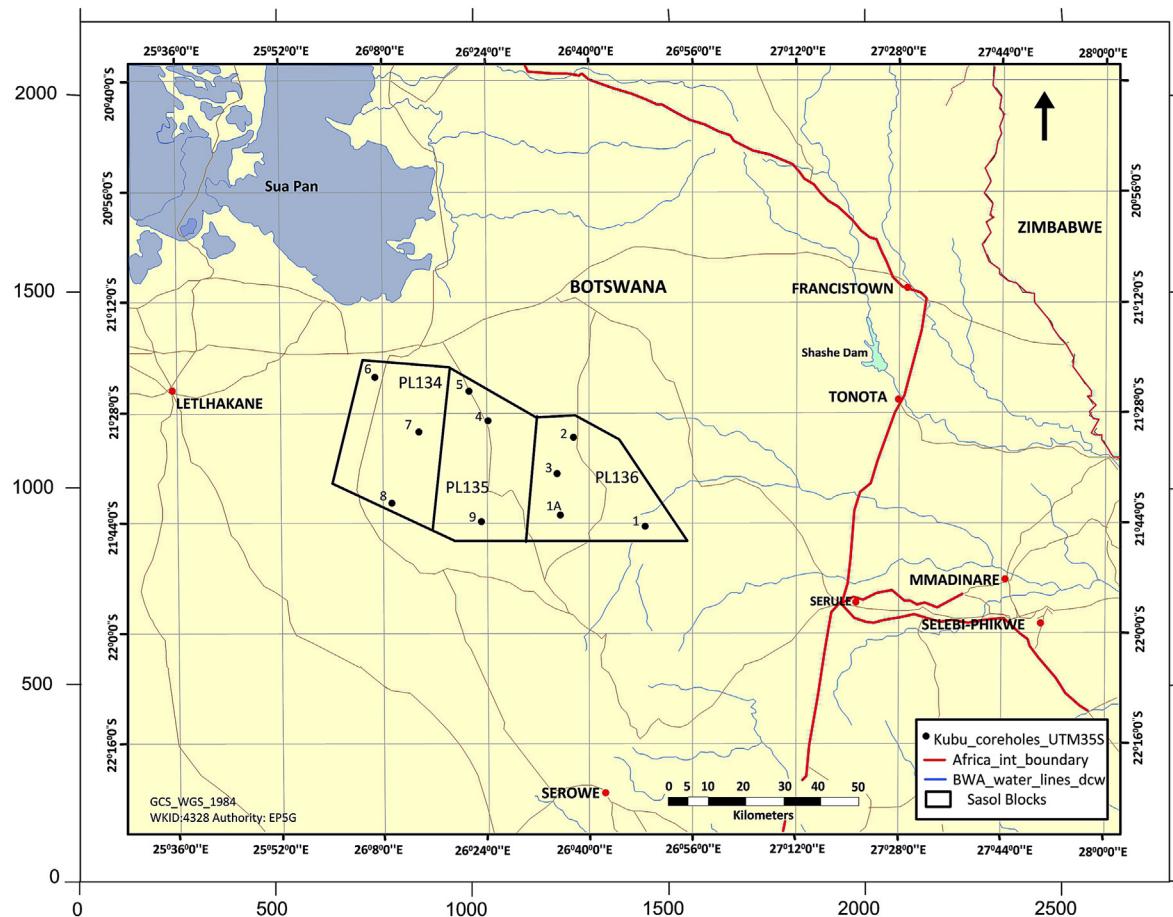


Fig. 1. Location of the nine exploration boreholes in central Botswana within Kudu licensed area (modified after Mabitje, 2016).

within the molecular structure of coal, and a small amount is stored as free gas in fractures and some in solution with water (Rao et al., 2014; Li et al., 2019; Singh et al., 2019; Tao et al., 2019). CBM may be accompanied by variable proportions of carbon dioxide and water, which are coal formation by-products (Singh, 2011; Rao et al., 2014; Zhu et al., 2019; Mendhe, 2020). The production of methane depends on the thickness, rank and maceral composition of the host coal. CBM occurs as biogenic (microbial) or thermogenic gas. Thermogenic gases have been associated with high rank coal, whereas microbial gases are produced at the early stages of the coalification process (Cokar et al., 2010; Rao et al., 2014; Song et al., 2018; Kalkreuth et al., 2020). The maceral composition of the Central Kalahari Karoo Basin's coal seams may have had a significant influence on the gas generation potential of the coal, dominated by vitrinite and inertinite groups with subsidiary quantities of liptinite; however, stratigraphically older coals contain less vitrinite and have higher inertinite contents (Bennett, 1989; Faiz et al., 2013; Bulguroglu and Milkov 2020).

The primary factor determining if a source rock can produce any hydrocarbons is thermal maturity (Shiri et al., 2013). Vitrinite reflectance (R_o) is the most commonly used maturation indicator of organic matter in sedimentary rocks. Vitrinite is a maceral group found in coals, in coaly inclusions in shales and disseminated in other sedimentary rocks. A method developed by Hood et al. (1975) for quantifying thermal maturity, which directly correlates to vitrinite reflectance, is the "level of organic metamorphism" (LOM). LOM is a scale that describes the degree of thermal metamorphism of organic matter with burial and it is used to measure the level of

maturity of organic matter (Hood et al., 1975). Temperature controls the conversion of kerogen to hydrocarbon molecules. The level of organic matter metamorphism is attributed to geological time and palaeogeothermal gradients resulting from uplift and erosion (Hood et al., 1975; Price, 1983; Singh et al., 2016). The coal rank provides a basic framework for studying the process of coalification. This framework is used effectively in comparing LOM stages in petroleum generating source rocks. The numerical scale to estimate the level of maturity of organic matter developed by Hood et al. (1975) ranges from zero, indicative of no burial to twenty, at the point of anthracite/meta-anthracite boundary, and covers the entire range from the onset of petroleum generation to its over-maturity stage (Hood et al., 1975; Singh, 2011; Yu et al., 2017; Yelwa et al., 2021).

Wireline logs are an inexpensive and available method to extract information relating to the subsurface conditions and rock properties (Rider and Kennedy, 2002; Ramiah et al., 2019; Saffou et al., 2020; Opuwari et al., 2022). It is common practice to use, amongst other methods, Passey's $\Delta\text{Log}R$ technique to evaluate total organic carbon (TOC) using resistivity and porosity logs (Passey et al., 1990; Shiri et al., 2013). In industry, the application of Passey's $\Delta\text{Log}R$ technique has proven to be a practical approach for estimating TOC in source rocks (Kamali and Mirshady, 2004; Zhu et al., 2019; Liu et al., 2021).

Passey's method involves the overlaying of an adequately scaled porosity log on a deep resistivity curve. Sonic and density logs are commonly used as the porosity indicator logs (Rider and Kennedy, 2002; Rider, 2002; Opuwari, 2010; Opuwari, 2010, 2010; Magoba

and Opuwari, 2020; Magoba and Opuwari, 2020, 2020; Ayodele et al., 2021). Sonic and resistivity log readings in low resistivity shale are referred to as the baseline readings (Asquith and Gibson, 1982). These readings will vary with the depth of burial and geologic age. This technique assumes that the baseline condition will occur at the non-source interval (Passey et al., 1990; Charsky and Herron, 2013; Sun et al., 2013; Yu et al., 2017).

This study examines if Passey's method can identify coal bearing rocks of the Central Kalahari Karoo Basin as organic carbon-rich zones. This method will also be used to quantify the TOC in the coal-bearing formations. Passey's calculated TOC percentage will be compared to the ultimate analysis's carbon measurements to test this technique's validity.

2. Geological background

The Kalahari Karoo basin is one of several southern African basins filled with Late Carboniferous to Jurassic sediment that are primary targets for Permian coal (Bordy et al., 2010a; Franchi et al., 2021). The basin covers approximately 70% of Botswana, trending Northeast-Southwest (Johnson et al., 1996; Modie and Le Hérisson, 2009; Franchi et al., 2021). It is divided into five sub-basins based on geological setting and facies changes (Smith, 1984). The Central Kalahari Karoo Basin is further sub-divided into southern, northern, western and south East Central Kalahari belts for descriptive purposes (Smith, 1984). This study's focus area is within the eastern part of Botswana (Fig. 1) in the Northern and South East Central Kalahari belts, within three production licenses (PL134, PL135 and PL136) in 2012–2013 (Faiz et al., 2013; Bulguroglu and Milkov 2020).

The Kalahari Karoo Basin and its subsidiary basins remain little understood in terms of their exact geodynamic setting. Some studies (Visser, 1997; Catuneanu et al., 2005; Haddon, 2005) have attributed these sub-basins to collision-induced extensional tectonics, related to the Late Palaeozoic to Early Mesozoic Gondwanide-Cape orogeny that resulted from the subduction of a palaeo-Pacific plate under southern Gondwana. This led to the Karoo Basin's development in the south as a retro-arc foreland basin to the Cape Fold Belt.

The Kalahari Karoo Basin's sub-surface structural framework is little understood due to the Kalahari Group sediments' extensive nature, generally 60–100 m thick and reaches 400 m thickness in the central Kalahari. Fault-bounded graben structures have been identified along the basin's eastern margin, exposed on the surface. The dyke swarm in central Botswana represents one of the significant fissure of intrusive complexes in the world (Le Gall et al., 2002). This complex forms a 1500 km long and 100 km wide tectono-magmatic structure extending from western Zimbabwe through Botswana and northern Namibia. The strike complex trends at 110° east. The individual dyke intrusions dip between 60 and 90° to the north-east. These dyke intrusions cut through Archaean basement terranes and Permo- Jurassic sedimentary sequences (Le Gall et al., 2002).

The stratigraphy of the Kalahari Karoo Basin records a transition from a glacial period to fluvio-deltaic and swampy periods and ultimately turns arid before the extrusion of continental flood basalts (Smith, 1984; Visser, 1997). The Kalahari Karoo Basin's stratigraphic nomenclature is adopted mainly from the South African Karoo stratigraphy it is well exposed (Smith, 1984; Catuneanu et al., 2005; Bordy et al., 2010b).

3. Materials and methods

This study's data includes wireline logs, proximate analysis results, and vitrinite reflectance measurements for exploration

boreholes CH1 to CH9. Vitrinite reflectance measurements were not conducted on all cored intervals, only four to five samples were selected per borehole. Vitrinite reflectance was used to determine thermal maturity on coal samples as this is an essential parameter in the TOC calculations.

Andersen Geological Consulting of South Africa conducted the geophysical logging of exploration boreholes (CH1–CH9). Wireline logs were provided for all nine boreholes, and they included gamma-ray (GR), density, resistivity and sonic logs.

The histogram distributions of log measurements were used to set a limit or baseline for different rock type classification. For example, a histogram distribution of GR logs for all boreholes, used to classify lithology types based on clay content, is presented in Fig. 2. The mean GR value, which is 113.27 °API, was used as a cut off value for differentiation. Below 113.27 °API, lithology was identified as dolerite, coal or sandstone or siltyclaystone. Above 113.27 °API, the lithology was considered as claystone. The density log distribution histogram served to segregate intervals with gamma-ray values less than 113.27 ° API into either dolerite, coal or silty mudstone. Table 1 shows log measurement ranges used to characterise lithology types (Amini et al., 2014; Mabitje, 2016; Opuwari et al., 2021; Opuwari and Dominick, 2021).

3.1. Proximate and ultimate analysis

Proximate analysis AS 1038.3 (Standards Association of Australia, 2000a) was conducted. The proximate analysis involves determining the volatile matter, moisture, fixed carbon and ash yield (Warne, 1991). The procedure involves drying a known mass of coal in an oxygen-free (nitrogen flush) oven at 105–110 °C for a period of 1.5–3 h (Mayoral et al., 2001). After removing the sample from the oven and placing it in a desiccator, the coal was weighed, and the loss of mass ascribed to inherent moisture measured. The sample is then heated in a cylindrical silica crucible in a muffle furnace at 950 °C for 7 min to effect the removal of all volatile matter. During this process, the loss of mass recorded is equal to the

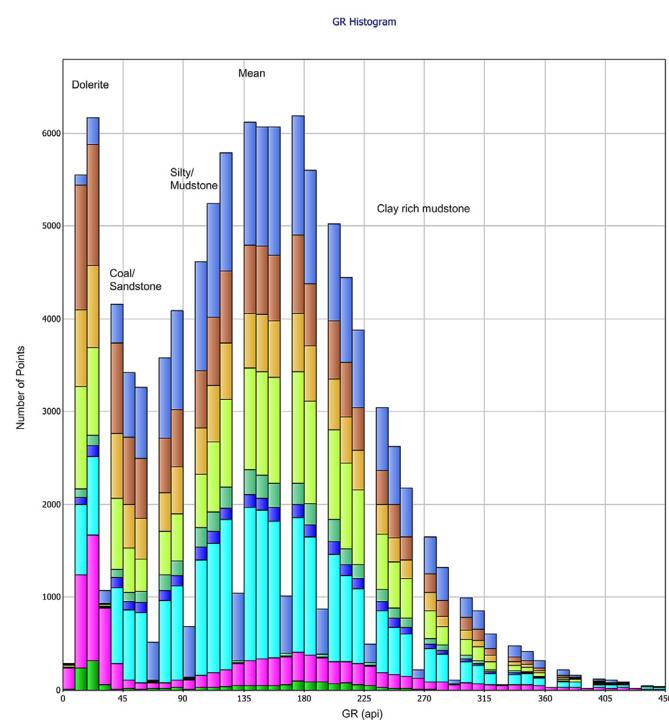


Fig. 2. Histogram distribution of clay content in all boreholes using gamma-ray curves.

Table 1

Approximate log measurement ranges used to characterise lithology types (modified after [Mabitje \(2016\)](#) and [Sahoo et al. \(2021\)](#)).

Lithology	Gamma-ray (°API)	Density (g/cc)	Resistivity (ohm-m)	Sonic (μsec/m)
Dolerite	3–21	2.7–3.2	110–1000	50–180
Coal	6–65	1.12–2.25	18–110	280–480
Silty Clastic	65–113	2.25–2.7	0.1–5	180–250
Clay rich	113–336	2.3–2.5	5–20	250–320

proportion of volatile matter present in the sample. Determination of ash yield is achieved by combusting the coal until a constant mass is attained by heating the sample to 500 °C for 30 min before increasing the temperature to 815 °C until combustion is complete. The ash percentage is calculated from the mass of the residue remaining after incineration. The amount of fixed carbon was not determined by direct measurement but calculated from the difference between the sums of all other components ([Elder, 1983](#)).

The ultimate analysis provides information on the elemental composition of coal, which are the proportions of carbon, hydrogen, nitrogen, oxygen, and sulphur for classification and application. For this analysis, a coal sample is combusted in an ultimate analyser, which measures the weight percentage of carbon, hydrogen, nitrogen, sulphur, and ash from a coal sample. The total carbon, hydrogen, and nitrogen are determined simultaneously from the same sample in the analyser. Total oxygen is calculated from the other values. The variations in chemical composition from the ultimate analysis data reflect variations in coal type and coal rank. The protocols from the testing method described by the Australian Standard for coal and coke analysis and testing method AS 2456.3 ([Standard Association of Australia, 2000b](#)) for ultimate analysis is used in this study.

3.2. Thermal maturity: vitrinite reflectance

Weatherford Laboratories conducted the vitrinite reflectance measurements according to the Australian Standards AS2456.3 ([Standards Association of Australia, 2000b](#)). A minimum of fifty readings were measured for each sample. Also, thermally affected samples displayed erroneous values and were noted in the report. Vitrinite reflectance measurements were then used to classify samples as immature, mature or post-mature, according to the ranking of [Diesel \(1992\)](#) and [Teichmüller \(1989\)](#) presented in [Table 2](#).

Passey's ΔLogR method requires LOM value to convert the ΔLogR separation to a quantitative TOC. To determine LOM values from R_o measurements, the R_o values were superimposed and

correlated with [Hood et al. \(1975\)](#) coal rank numerical scale ([Fig. 3](#)) and equivalent LOM value obtained. The coal rank scale is from zero at burial to twenty, and it is subdivided within the sub-bituminous and high volatile bituminous coal rank classification. The estimated LOM with respect to vitrinite reflectance of the samples is presented in [Table 3](#). The vitrinite reflectance was plotted as a function of LOM ([Fig. 4](#)), and a relationship for the estimation of LOM from R_o was established as follow:

$$\text{LOM} = 0.004 (R_o^3) - 0.4987 (R_o^2) + 5.1115 (R_o) + 5.5714 \quad (1)$$

Using the relationship between LOM and R_o established in [Fig. 4](#), [Table 3](#) was created to assign R_o measurements their corresponding LOM values. Based on the established correlation, a LOM value less than 8.46 correlates to thermally immature coal, and LOM values ranging from 8.46 to 10.59, 10.59–11.76, and greater than 11.76 correspond to the oil window, the wet gas/condensate window, and the dry gas window, respectively.

3.3. Passey's method and input parameters

Passey's method for the determination of TOC uses the density, sonic, and deep resistivity curves. The density and sonic curves are individually overlain with the deep resistivity curve in an organic lean interval, and the overlap is defined as the baseline ([Yu et al., 2017](#)). A baseline exists when there is an overlap between two curves, resistivity/density and resistivity/sonic, or when the curves are close to each other in a relatively thick interval. An organic-rich source rock interval is recognised by a separation of the two curves ([Fig. 5](#)). The separation between the density/resistivity and sonic/resistivity is designated as Δlog R, which is related to TOC, and it can be measured at different depth intervals ([Passey et al., 1990](#)).

The baseline interval readings of 10 Ω m, 2.5 g/cc, and 300 μs/m were recorded for resistivity, density, and sonic logs, respectively. The sonic, density and resistivity logs were used to achieve DlogR (density resistivity) and SlogR (sonic resistivity) separations. These separations were quantified and then used together with individual

Table 2

Phases of petroleum generation with their corresponding vitrinite reflectance indices ([Diesel, 1992](#); [Teichmüller, 1989](#)).

Coal Rank	R_o (%)	LOM	Maturity Phase
Peat	<0.23	<6.72	Immature
Lignite	0.23–0.36	6.72–7.35	Immature
Sub-bituminous: C	0.36–0.41	7.35–7.58	Immature
Sub-bituminous: B	0.41–0.47	7.58–7.86	Immature
Sub-bituminous: A	0.47–0.49	7.86–7.96	Immature
High-Volatile Bituminous: C	0.49–0.51	7.96–8.05	Immature
High-Volatile Bituminous: B	0.51–0.69	8.05–8.86	Immature to Mature
High-Volatile Bituminous: A	0.69–1.11	8.86–10.64	Mature (Oil)
Medium-Volatile Bituminous	1.11–1.6	10.64–12.49	Mature(wet gas)
Low-Volatile Bituminous	1.6–2.04	12.49–13.96	Mature (dry gas)
Semi-Anthracite	2.04–2.4	13.96–15.02	Mature
Anthracite	2.4–5	15.02–19.16	Mature to Post Mature
Meta-Anthracite	>5	>19.16	Post Mature

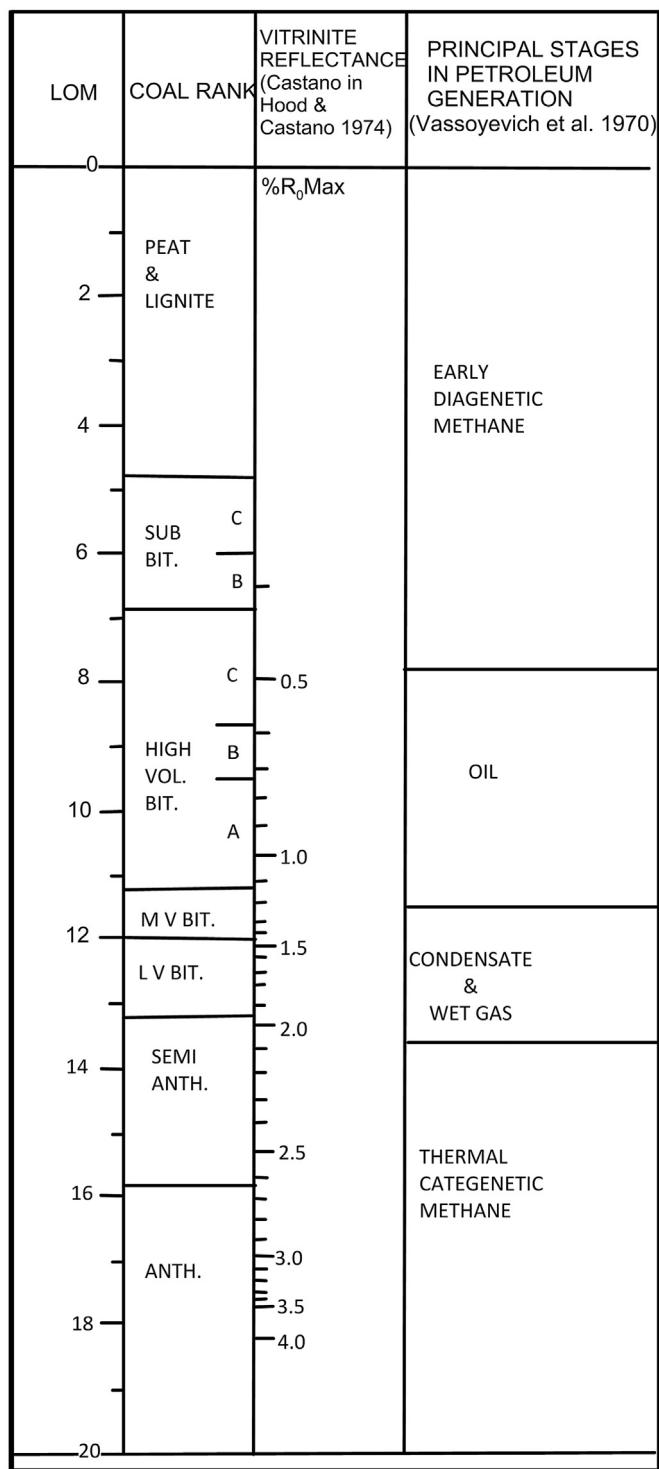


Fig. 3. Numerical scale relating coal rank, vitrinite reflectance (R_o) and petroleum generation stage to level of organic metamorphism (LOM) (modified after Hood et al., 1975).

LOM values as inputs in the TOCd (TOC calculated from density log) and TOCs (TOC calculated from the sonic log) calculations in Microsoft Excel. For the generation of TOC curves in IP Software, the same inputs were used, but instead of inserting raw data averages from spreadsheet listings in the equation, actual resistivity, density and sonic curves were used.

4. Results and discussion

4.1. Thermal maturity

The R_o for all samples analysed indicate a wide range of measurements, from 0.4 to 5.53 (Fig. 6a). The geothermal gradient in the basin is approximately $36\text{ }^{\circ}\text{C/km}$ (Haddon, 2005). The R_o in CH1 and CH6 are between 0.44 and 0.65, indicating that coal in both boreholes is low to medium rank. Also, R_o increases with depth (Fig. 6) in these boreholes, signifying the role played by diagenesis. These boreholes can be used for control and comparison of % Ro in boreholes affected by intrusions.

In boreholes CH2, CH3, CH4, CH5, CH7, CH8 and CH9, some coal intervals are affected by the heating from dolerite intrusions. The heating from dolerite intrusions is evident in their % Ro measurements ranging between 0.77% and 5.53% (Fig. 6). Intrusion on coal has been proven to increase the vitrinite reflectance values (Bostick and Pawlewicz, 1984; Stewart et al., 2005; Fjeldskær et al., 2008). Coals in closest contact with intrusions show $R_o > 5\%$, which rapidly decreases to 0.77% with increasing distance from the intrusion. This rapid decrease in R_o suggests that intrusive events' contact metamorphism was probably confined to a few meters on either side of intrusion. The alteration of coal is highest at the contact and extends into the coal as an aureole (Golab, 2003; Jiang et al., 2011). The aureole size depends on the chemistry, temperature, degree of intrusion crystallisation, and volatile fluids (Golab, 2003).

Bennett (1989) found that coals of the Mamabula area in the Central Kalahari Karoo Basin have a mean maximum R_o between 0.52 and 0.64. He attributed the immaturity of the coals to the basin dynamics and burial depths. The R_o measurements of his study are consistent with CH1 and CH6, measured between 0.44 and 0.65. The borehole's R_o values indicate that coals in the basin are primarily sub-bituminous type B to high volatile bituminous type B in rank. High volatile bituminous to anthracitic coals formed by rapid heating that occurred in localised areas adjacent to intrusions. In Table 3, samples at depth 374.10 m and 410.25 m of borehole CH3 are not thermally metamorphosed, whereas intervals above and below them are heat affected. Heat effects depend on the extent of the contact aureole for each sill.

Based on R_o measurements and distance between coal intervals and sill in each borehole, the sill intrusion area is divided into three zones: (1) contact metamorphism zone, which is within 2–12 m from the sill, (2) thermal evolution zone, that is within distances of 12–54 m from the sill and (3) unaltered zone. The contact metamorphism zone displays R_o from 3.67% up to 5.53%; the thermal evolution zone has R_o between 0.77% and 1.91. The unaltered zone is characterised by R_o of between 0.44% and 0.65.

The heat affected samples are mostly mature, covering the oil, wet gas and condensate and dry gas windows. Their LOM ranges from 9.21 to 19.26, with post-mature samples yielding values more significant than 18.29. Heat effects accelerated the LOM of these coals. Non-heat affected samples from all boreholes show LOM values ranging from 7.72 to 8.68, and these are considered immature (Table 3). Corresponding LOM values in terms of the three zones of the intrusion area are 7.72–8.68, 9.21–13.54 and >17.81 for the unaltered, thermal evolution and contact metamorphism zones, respectively (Fig. 6b).

Similarly, with R_o , boreholes CH1 and CH6 display increasing LOM and rank with depth. In intruded boreholes CH2 and CH8 (Table 3), there is an increase of LOM with depth, probably because sill intrusions in both boreholes only occur adjacent to deeper sampled intervals. Therefore, an alteration was only experienced in these intervals governed by aureole dynamics where the coals in contact or adjacent to the intrusion will be heated the most. The intrusions have altered the relationship between maturity and

Table 3A quantitative relationship between coal rank, R_o , LOM and indication of coal rank and maturity phases.

Borehole	Depth m	Coal Rank	VRo %	LOM	Maturity Phase
CH1	246.12	Sub-bituminous: B	0.44	7.72	Immature
CH1	268.80	Sub-bituminous: B	0.47	7.86	Immature
CH1	275.50	Sub-bituminous: A	0.49	7.96	Immature
CH1	277.76	Sub-bituminous: B	0.47	7.86	Immature
CH1	279.9	High-Volatile bituminous C	0.5	8.00	Immature
CH2	257.64	Sub-bituminous: B	0.46	7.82	Immature
CH2	272.49	High-Volatile Bituminous:A	0.77	9.21	Mature
CH2	276.51	Medium Volatile Bituminous	1.52	12.20	Mature
CH2	297.20	DOLERITE			
CH2	357.97	Medium Volatile Bituminous	1.57	12.38	Mature
CH3	364.37	High-Volatile Bituminous:A	0.83	9.47	Mature
CH3	374.10	High-Volatile Bituminous:B	0.52	8.10	Immature
CH3	410.25	High-Volatile Bituminous:B	0.64	8.64	Mature
CH3	418.44	High-Volatile Bituminous:A	0.92	9.85	Mature
CH3	421.46	Medium Volatile Bituminous	1.39	11.72	Mature
CH3	431.70	DOLERITE			
CH4	381.00	Low Volatile Bituminous	1.91	13.54	Mature
CH4	392.00	DOLERITE			
CH4	438.25	Meta Anthracite	5.53	19.26	Post Mature
CH4	451.19	High-Volatile Bituminous:A	0.84	9.52	Mature
CH4	479.97	High-Volatile Bituminous:A	0.87	9.64	Mature
CH4	488.31	Medium Volatile Bituminous	1.59	12.45	Mature
CH6	319.78	Sub-bitumonous: B	0.45	7.86	Immature
CH6	329.01	High-Volatile Bituminous:C	0.51	8.05	Immature
CH6	420.22	High-Volatile Bituminous:B	0.60	8.46	Mature
CH6	356.27	High-Volatile Bituminous:B	0.65	8.68	Mature
CH7	404.28	High-Volatile Bituminous:C	0.50	8.00	Immature
CH7	432.92	High-Volatile Bituminous:B	0.54	8.19	Immature
CH7	440.22	High-Volatile Bituminous:B	0.54	8.19	Immature
CH7	462.81	High-Volatile Bituminous:B	0.55	8.23	Immature
CH7	485.62	Anthracite	3.88	18.13	Mature
CH7	500.40	DOLERITE			
CH8	374.29	Sub-Bituminous -C	0.40	7.54	Immature
CH8	386.81	High-Volatile Bituminous:B	0.62	8.55	Mature
CH8	391.07	High-Volatile Bituminous:A	0.90	9.77	Mature
CH8	419.00	DOLERITE			
CH9	406.40	High-Volatile Bituminous:C	0.51	8.05	Immature
CH9	419.60	DOLERITE			
CH9	421.30	Anthracite	3.67	17.81	Mature
CH9	444.60	Medium Volatile Bituminous	1.30	11.38	Mature
CH9	455.90	DOLERITE			
CH9	504.60	Anthracite	4.71	19.00	Post Mature
CH9	520.86	Low Volatile Bituminous	1.88	13.44	Mature
CH9	525.90	DOLERITE			

depth in boreholes CH3, CH4, CH5 and CH9.

4.2. Proximate and ultimate analysis

The proximate analysis performed to determine the ash yield, moisture, volatile matter, and fixed carbon at the air-dry base and dry ash-free basis are presented in Table 4. The results indicate three clusters (Fig. 7) in the sample distribution. Cluster 1(green colour) is non-heat affected with R_o ranging from 0.44% to 0.65%. Cluster 2 (blue colour) samples are slightly heated to heat-affected with R_o ranging between 0.77% and 1.91%. Cluster 3 (red colour) is the devolatilized or coked coal samples with R_o and greater. These clusters correspond to the three zones distinguished earlier. Cluster 1 displays the highest moisture content range from 2.42% to 6.36%, in cluster 2, the range is from 0.76% to 3.14%, and cluster 3 ranging from 1.3% to 3.4%. Surprisingly, the moisture of the slightly heat-affected samples is less than that of the devolatilized samples. According to Jiang et al. (2011), this may occur due to the intrusion acting as a seal to prevent moisture loss after the magmatic intrusion. This observation may hold as the devolatilized samples are within the contact metamorphism zone (2–12 m from nearest sill).

Cluster 3 displays the lowest volatile matter content proving that with increasing heat effects from intrusion, devolatilisation occurs. Thermally evolved cluster 2 shows higher fixed Carbon than cluster 1. These results are generally in agreement with those of Jiang et al. (2011) and (Rimmer et al., 2009), who both state that intrusions on coal seams result in increases in fixed Carbon and % R_o and decreases volatile matter and moisture adjacent to the igneous intrusion. Cluster 3 exhibits a decrease in fixed Carbon and an increase in ash yield with increasing R_o . According to Golab (2003), this is because, at higher temperatures where coking begins, vitrinite becomes porous, changes from anisotropic to isotropic and crystallises to form semi-coke. The liptinites spontaneously decompose, reflectance increases and all or part of the organic matter is removed by reactions that form carbon dioxide, methane and other products.

An exception in cluster 3, sample at depth 486.2 m of borehole CH7, interpreted as an anthracite coal rank with R_o of 3.88 (Tables 3 and 4), displays the highest fixed carbon measurement of 67.18% and 22.10% ash content at air-dry basis, this is possible because it has not reached the post maturity phase of $R_o > 4$ and is in an early stage of semi-coking.

The ultimate analysis results found that the carbon percentage

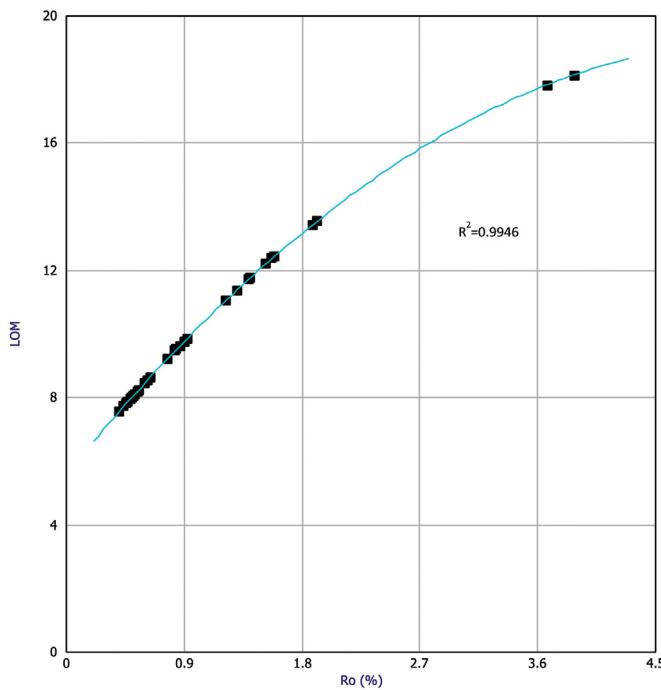


Fig. 4. Graphical representation of the relationship between R_o and LOM.

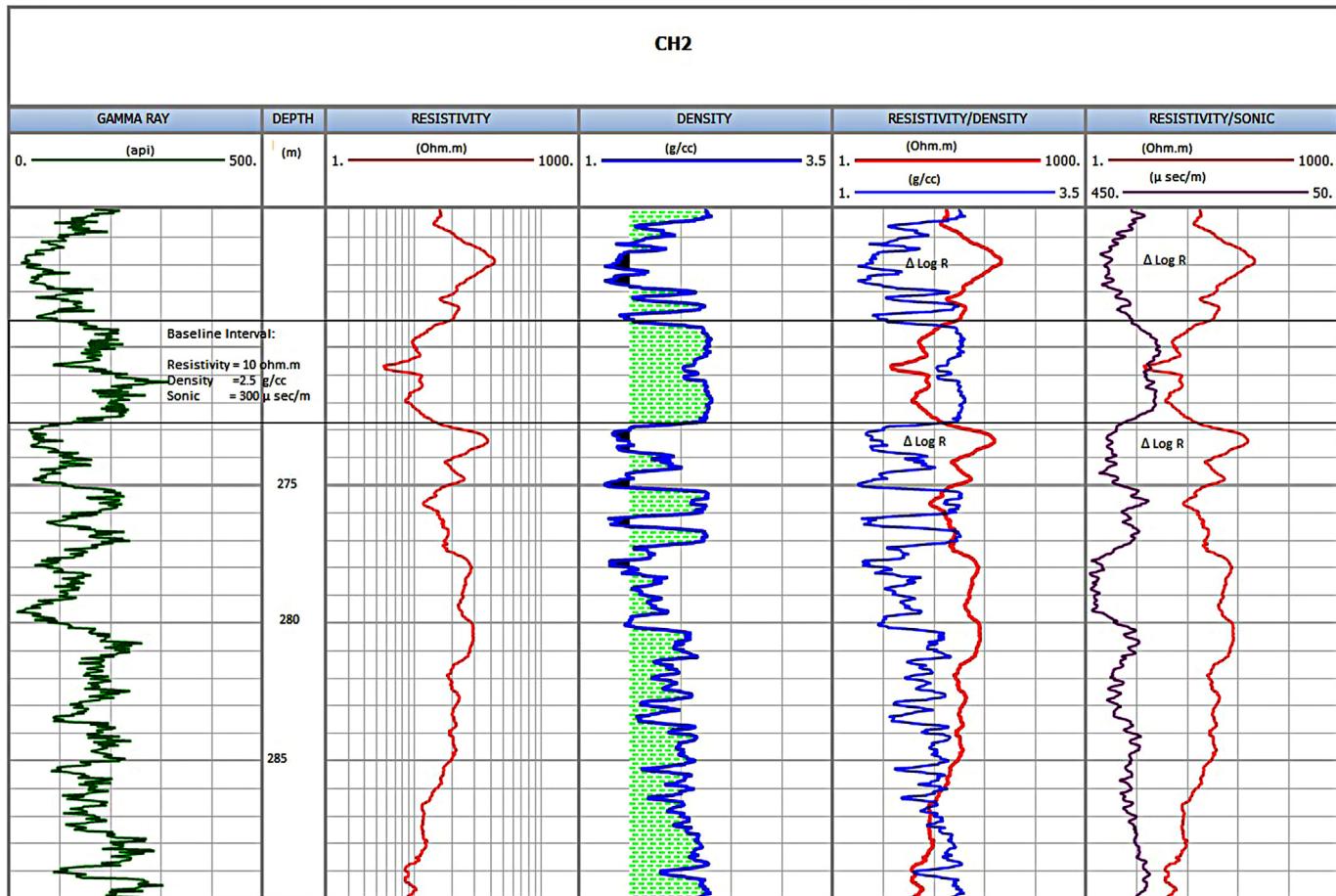


Fig. 5. Example of logs used to establish a baseline. The separation of the two curves recognises an organic-rich source rock interval. Gamma-ray log plotted in track 1, while the overlay of resistivity and density log is displayed in track 5, and overlay of resistivity and sonic logs are displayed in track 6.

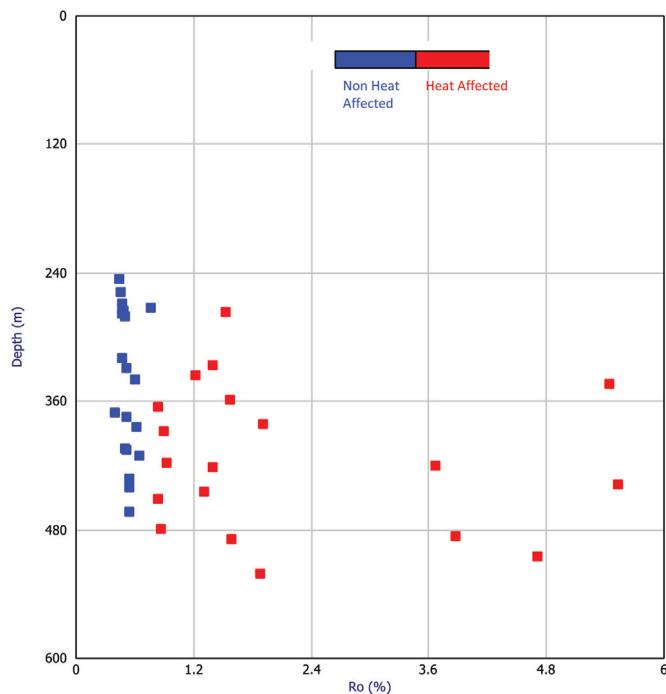


Fig. 6. Vitrinite reflectance (R_o) distribution with depth for all boreholes. R_o trends with depth for coals heat-affected by dolerite intrusions and non-heat affected coals.

Table 4
Proximate analysis results of boreholes.

Borehole	Depth m	M % ad	A % ad	VM % ad	FC % ad	M % daf	VM % daf	FC % daf
CH1	245.82	5.65	22.11	28.74	43.49	7.25	36.90	55.84
CH1	268.38	5.45	20.23	31.50	42.82	6.83	39.49	53.68
CH1	275.24	5.43	21.04	30.70	42.84	6.88	38.88	54.26
CH1	277.30	4.71	29.99	25.84	39.46	6.73	36.91	56.36
CH1	279.96	5.08	12.37	32.94	49.62	5.80	37.59	56.62
CH2	257.64	4.88	26.79	33.52	34.82	6.67	45.79	47.56
CH2	272.49	2.69	26.84	27.69	42.78	3.68	37.85	58.47
CH2	276.51	1.45	21.45	16.30	60.81	1.85	20.75	77.42
CH2	297.20		DOLERITE					
CH2	357.97	0.76	34.45	18.77	46.02	1.16	28.63	70.21
CH5	247.77	1.85	24.56	22.65	50.94	2.45	30.02	67.52
CH5	268.40		DOLERITE					
CH5	283.00	2.43	48.50	6.57	42.50	4.72	12.76	82.52
CH5	294.30		DOLERITE					
CH5	325.77	2.21	31.35	23.61	42.83	3.22	34.39	62.39
CH5	335.26	1.37	17.26	22.11	59.25	1.66	26.72	71.61
CH5	344.10	2.27	57.05	8.38	32.30	5.29	19.51	75.20
CH6	319.59	5.99	42.21	23.38	28.41	10.37	40.46	49.16
CH6	328.84	5.27	16.07	34.62	44.04	6.28	41.25	52.47
CH6	340.05	4.98	13.60	32.00	49.41	5.76	37.04	57.19
CH6	355.50	2.42	63.10	13.18	21.30	6.56	35.72	57.72
CH7	403.83	6.36	29.78	32.85	31.01	9.06	46.78	44.16
CH7	462.86	3.72	12.91	32.05	51.33	4.27	36.80	58.94
CH7	485.62	1.30	22.10	9.42	67.18	1.67	12.09	86.24
CH9	405.70	3.81	39.94	22.04	34.21	6.34	36.70	56.96
CH9	419.60		DOLERITE					
CH9	420.80	1.52	58.09	6.03	34.37	3.63	14.39	82.01
CH9	444.21	1.91	40.61	15.51	41.97	3.22	26.12	70.67
CH9	455.90		DOLERITE					

M% (ad) moisture present percentage in dry basis, A(ad)% ash present in dry basis, VM(ad)% volatile matter present percentage in dry basis, FC(ad)% fixed carbon present percentage in dry ash-free basis, M%(daf) moisture present in dry ash-free basis, VM(daf)% volatile matter present percentage in dry ash-free basis, FC(daf)% fixed carbon present percentage in dry ash-free basis.

4.3. The Passey's TOC outputs

Passey's method has been extensively utilised to determine the organic richness of rock. Passey's TOCs and TOCd were determined using equations:

$$\text{TOCs} = \text{SlogR} * 10^{(0.297 - 0.1688 * \text{LOM})} \quad (2)$$

$$\text{TOCd} = \text{DlogR} * 10^{(0.297 - 0.1688 * \text{LOM})} \quad (3)$$

Borehole CH1 did not intercept any dolerite, all samples are immature, but high resistivity responses observed at depth 275.0 m–277.30 m indicate early biogenic gas generation. The correlation between Carbon at dry ash-free (daf %) and calculated TOC of boreholes CH1 and CH7 of the non-heat affected and heat affected boreholes (Fig. 8) showed that TOCs calculated from the sonic log displayed a better correlation than that of density log (TOCd). A coefficient of determination of $R^2 = 0.85$ (CH1) and 0.48 (CH7) was determined from TOCs, whereas the TOCd calculated from the sonic log showed a coefficient of determination of 0.47(CH1) and 0.25 (CH7), respectively.

The heat affected samples at depth 276.51 m and 357.97 m of borehole CH2 showed very high LOM (Table 3) and a high value of fixed carbon (Table 4). This can also be observed in heat-affected samples of all the other boreholes. The sample at depth 357.97 m has been metamorphosed to hard carbonaceous coal; this, coupled with a comparatively higher LOM, has immensely affected the TOC outputs.

Passey et al. (1990) stated that TOCs accuracy is superior to logs TOCd and suggested that this could be due to the sensitivity of density logs to adverse hole conditions and heavy minerals such as pyrite. In this study, TOCs do not display any superiority to TOCd; its accuracy is poorer than TOCd. The density of the samples controls both density and sonic log readings. Most sampled intervals are pyritic and do not necessarily exhibit higher densities due to their presence. Passey's method is helpful in identifying coal as organic-rich zones and potential source rocks. However, accuracy in its TOCs/TOCd predictions depends on selected baseline readings, density and more so, on the LOM of the coal. LOM has proved to be a significant and sensitive parameter in this method.

Coal that has undergone normal burial metamorphism compositionally varies from the rapidly heat altered coal. The R_o increased from 0.44 in non-heat affected coal to 5.53 in the contact metamorphism zone (Table 3). Adjacent to the intrusion, there is a decrease in the volatile matter; moisture initially decreases then slightly increases as sealed by the intrusion; the fixed carbon initially increases then decreases as vitrinite decomposes and semi-coke begins to form. Ash yield increases adjacent to the intrusion. According to Rimmer et al. (2009), these geochemical changes reflect increasing rank approaching the intrusion.

4.4. Application of Passey's ΔLogR : generating TOC curves

The vitrinite reflectance measurement was conducted on 41 cored intervals. In the remaining intervals, LOM is estimated; however, this has been done in boreholes CH1 and CH6, where maturity is believed to have been due to the normal coalification process. LOM ranges are 7.72–8 and 7.86 to 8.68 for CH1 and CH6, respectively (Table 3). Therefore, in both boreholes, an average LOM value within a reasonable range can be used to generate TOC estimation curves for the entire borehole. In dolerite heat influenced boreholes, using an average LOM would lead to very erroneous TOC

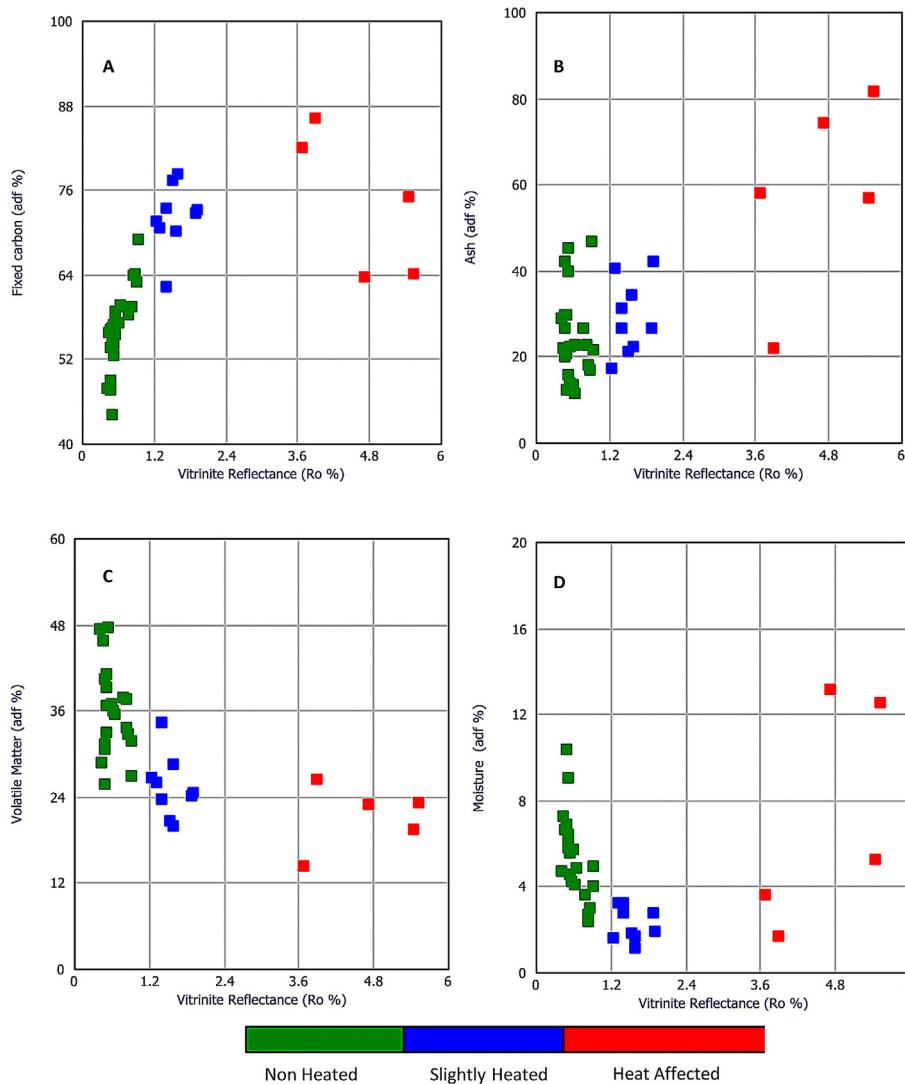


Fig. 7. Correlations between R_o and proximate analysis results. (a) Fixed Carbon Vs R_o , (b) ash content Vs R_o , (c) volatile matter Vs R_o , and (d) Moisture content Vs R_o . Cluster 1(green colour) represents non-heat affected, cluster 2 (blue colour) represents slightly heat-affected, and Cluster 3 (red colour) represents devolatilized heat-affected samples.

estimates as the LOM ranges are too broad and are not depth dependant. For example, CH4 and CH7 display LOM ranges of 9.52–19.26 and 8 to 18.13, respectively.

Fig. 9 and **Fig. 10** (track 7) indicate that TOCs estimations are more robust than TOCd in both boreholes. Essentially in both boreholes, Passey's TOC curves mostly align well with the carbon measurements. Although not accurate, the curves indicate that the method can be applied to coal that has not been thermally altered by igneous sills and dykes.

5. Conclusions and recommendations

Passey's method is successfully used to determine total organic carbon (TOC) from boreholes in Botswana's Kalahari Basin. Results of Passey's method compared with laboratory-measured carbon showed that Passey's method effectively identifies coal intervals. However, the method works poorly in coal metamorphosed by

dolerite intrusions. The heat affected coal samples had R_o from 0.77 to 5.53 and increased in maturity from primary maceral controlled to high volatile bituminous and anthracite coal. Proximate analysis showed compositional changes in the coal were controlled by proximity to sill intrusion, with a decrease in Fixed Carbon and an increase in ash yield in the contact metamorphism zone. The method works well for the unaltered coal that has undergone burial maturation displaying R_o of 0.44–0.65. In unintruded boreholes, correlations between carbon and calculated TOC indicate strong relationships. This study has demonstrated that TOC calculated from the sonic log is more reliable in coal not affected by contact metamorphism than TOC calculated from the density log.

One of the significant shortcomings of Passey's method is selecting the subjective baseline interval. Also, heterogeneity of shale sequences could result in high uncertainties for calculated TOC. Although coals generally have high carbon contents, it is possible that minor carbonate quantities may have contributed to

Table 5

Ultimate analysis results.

Borehole	Top Depth (m)	Carbon (% d.a.f)	Hydrogen (% d.a.f)	Nitrogen (% d.a.f)	Sulphur (% d.a.f)	Oxygen (% d.a.f)	H/C	O/C
CH1	245.82	76.1	5.05	1.53	1.9	15.4	0.07	0.20
CH1	268.38	76.7	4.92	1.5	2.7	14.2	0.06	0.19
CH1	275.24	77.8	4.71	1.57	1.56	14.4	0.06	0.19
CH1	277.30	74.7	4.97	1.61	3.2	15.5	0.07	0.21
CH1	279.96	76.6	5.12	1.69	2.69	13.9	0.07	0.18
CH3	364.70	79.5	4.88	1.46	3.04	11.1	0.06	0.14
CH3	374.94	71.8	5.52	1.58	1.66	19.4	0.08	0.27
CH3	410.45	78.5	4.58	1.68	0.6	14.6	0.06	0.19
CH3	417.95	83.4	3.74	2.17	2.59	8.1	0.04	0.10
CH3	420.95	85.1	3.87	2.06	0.48	8.5	0.05	0.10
CH5	247.77	80.3	4.94	1.14	6.62	6.7	0.06	0.08
CH5	283.00	91	1.25	0.64	3.04	4.1	0.01	0.05
CH5	325.77	78.8	4.63	1.78	1.03	13.8	0.06	0.18
CH5	335.26	84.8	4.28	1.92	0.87	8.1	0.05	0.10
CH5	344.10	85.7	2.84	1.16	0.24	10.1	0.03	0.12
CH6	319.59	73.2	5.44	1.25	5.61	14.5	0.07	0.20
CH6	328.84	78	5.31	1.49	1.97	13.2	0.07	0.17
CH6	340.05	77.3	4.93	1.68	0.65	15.4	0.06	0.20
CH6	355.50	71.1	5.51	1.38	0.35	21.7	0.08	0.31
CH7	403.83	75.9	4.87	1.46	2.82	15	0.06	0.20
CH7	432.36	78.4	5.14	1.54	1.15	13.8	0.07	0.18
CH7	439.95	78.5	5.22	1.72	0.75	13.8	0.07	0.18
CH7	462.86	79.1	5.04	1.95	0.85	13.1	0.06	0.17
CH7	485.62	89.3	2.95	1.8	1.19	4.8	0.03	0.05
CH8	370.48	75.3	5.39	1.51	10.55	7.3	0.07	0.10
CH8	383.62	79.6	5.12	1.6	2.95	10.7	0.06	0.13
CH8	387.88	80.7	5.17	1.16	2.43	10.1	0.06	0.13
CH9	405.70	74.7	5.26	1.48	5.27	13.3	0.07	0.18
CH9	420.80	87.8	3.48	1.92	0.55	6.3	0.04	0.07
CH9	444.21	83.9	4.62	1.92	2.2	7.4	0.06	0.09
CH9	504.60	76.7	4.23	1.34	0.61	17.1	0.06	0.22
CH9	520.86	83.5	4.38	1.99	4.03	6.1	0.05	0.07

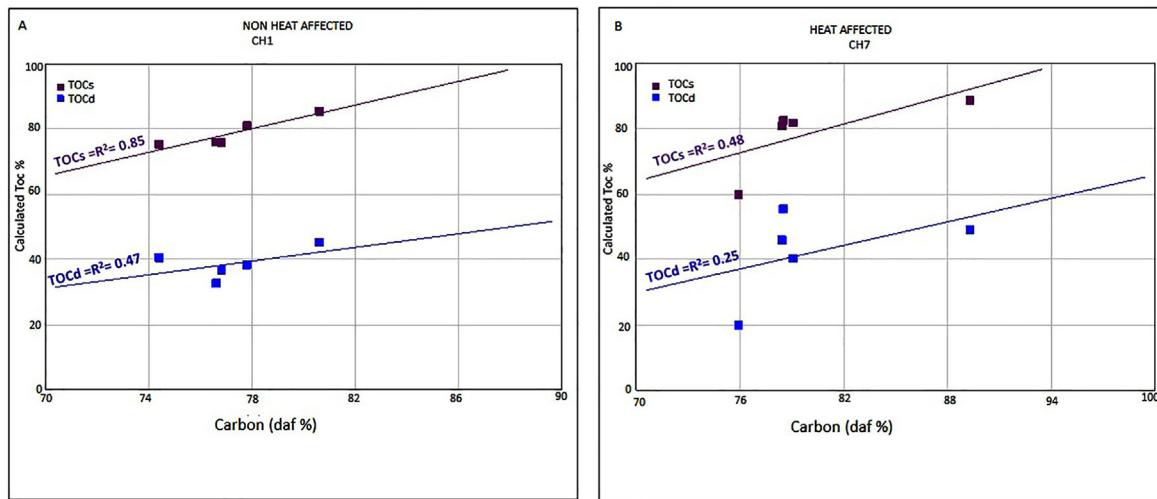


Fig. 8. Plot of calculated TOC against the fixed carbon (daf%) for non-heat-affected and heat-affected boreholes. (a) Non-heat-affected borehole (CH1) presenting an excellent relationship between calculated TOCd and fixed carbon and fair TOCs. (b) The heat affected (CH7) presenting a fair and poor relationship between TOC and fixed carbon.

the total carbon amount and may be the cause of inaccuracy in some calculated TOC using the ΔLogR technique as it only detects organic carbon. Thus, it is recommended that Rock-Eval pyrolysis be conducted on decarbonated coal samples to provide direct TOC measurements.

Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

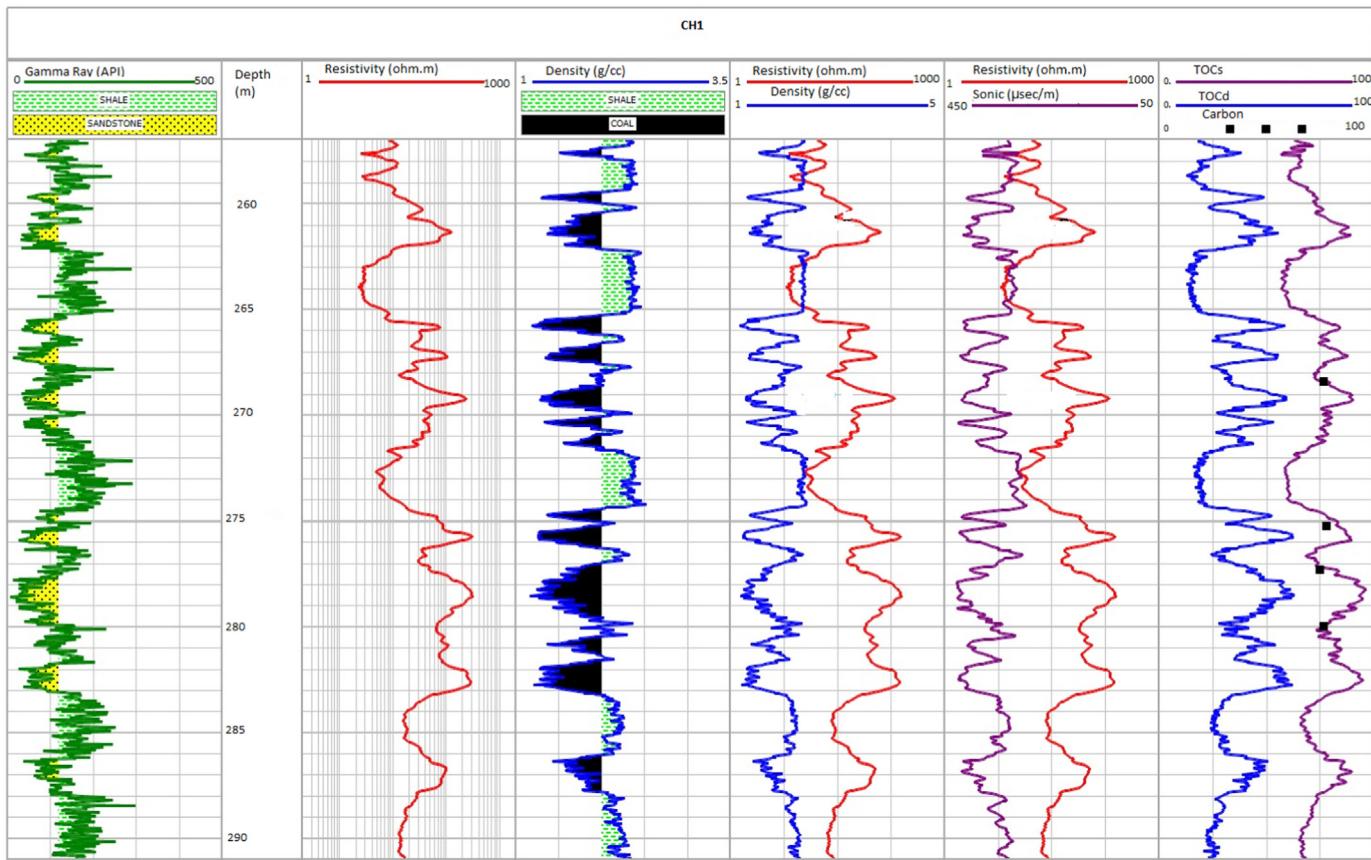


Fig. 9. Present log evaluation results for TOC for borehole CH1 (non-heat affected). The 1st track is GR, and the 2nd track is the depth curve. The 3rd track shows the resistivity, and the 4th track shows the density curve. The 5th track is the overlay of resistivity with density, and the 6th track is the overlay of resistivity with the sonic curve. The 7th track shows a comparison of TOCd, TOCs curves and fixed carbon (black dots). Good agreement between TOCd and fixed carbon was observed, indicating the effectiveness and reliability of the TOCd in non-heat affected coal.

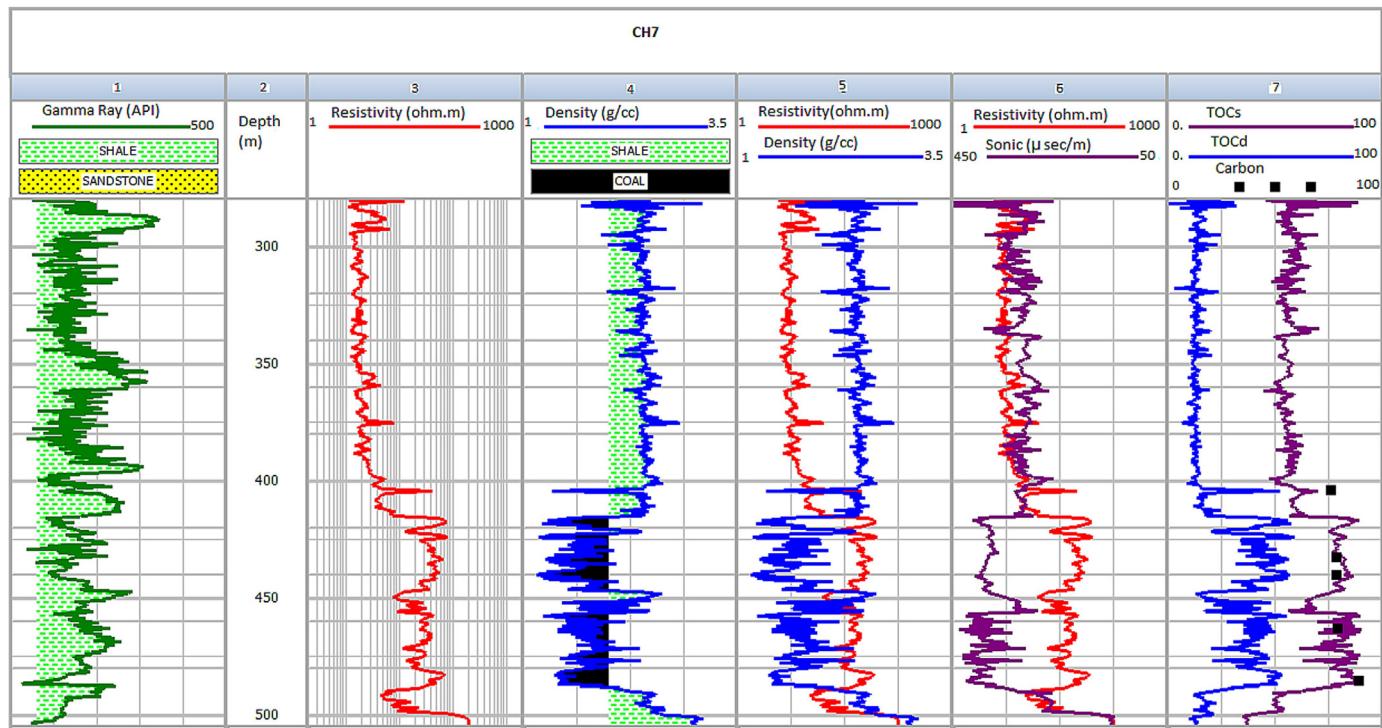


Fig. 10. Presentation of log evaluation results for TOC for borehole CH7 (heat affected). The 1st track is GR, and the 2nd track is the depth curve. The 3rd track shows the resistivity, and the 4th track shows the density curve. The 5th track is the overlay of resistivity with density, and the 6th track is the overlay of resistivity with the sonic curve. The 7th track shows a comparison of TOCd, TOCs curves and fixed carbon (black dots). The data show poor agreement between TOCd and fixed carbon, thereby indicating the unreliability of the TOCd in heat-affected coal.

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